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基于量子点光放大器波长转换的啁啾特性研究

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摘要: 信号光的啁啾特性在很大程度上会影响量子点半导体光放大器(QD-SOA)的性能,引起传输信号的走离效应,使误比特率增高。为了改善这一特性,对QD-SOA全光波长转换器的啁啾特性进行了系统分析,基于QD-SOA的交叉增益调制效应的全光波长转换原理,采用牛顿法和4阶龙格-库塔法求解速率方程和光场传输方程,计算了注入电流、抽运光脉宽和抽运光消光比变化时QD-SOA全光波长转换器输出变换光的啁啾值。结果表明,增大抽运光脉宽、减小注入电流和抽运光消光比均可减小变换光的啁啾值,通过优化这些参量可以减小啁啾的影响,但在设计QD-SOA全光波长转换器时,要考虑抽运光消光比和变换光啁啾之间的均衡。

关键词: 光通信; 量子点光放大器; 啁啾; 交叉增益调制

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Theoretical study on chirp of wavelength conversion based on QD-SOA

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Abstract: Chirp characteristics of signal light can largely affect the performance of quantum-dot semiconductor optical amplifiers (QD-SOA), cause the walk-off effect of transmitted signal and increase the bit error rate. To improve this situation, chirp characteristics of QD-SOA all-optical wavelength converters were analyzed. Based on all-optical wavelength conversion principle of QD-SOA's cross-gain modulation (XGM), using Newton's method and 4-order Runge-Kutta method, rate equations and light field transmission equation were solved, chirp values of converted light of a QD-SOA all-optical wavelength converter were calculated with the change of injection current, pumping light pulse width and extinction ratio of pumping light. The results show that increasing pulse width of pumping light, reducing injection current and extinction ratio of pumping light can reduce the chirp value of converted light. The impact of chirp can be reduced by optimizing these parameters. But during the design of QD-SOA all-optical wavelength converters, the balance between extinction ratio of pump light and chirp of conversion light should be considered.

Key words: optical communication; quantum-dot semiconductor optical amplifier; chirp; cross-gain modulation

引言

随着不断增长的通信容量需求,现代通信网的发展趋势是全光网络,这要求其中的光学器件具有高速的信号处理速度和能力。一般量子点半导体光放大器(quantum-dot semiconductor optical amplifier, QD-SOA)

与传统半导体光放大器(bulk semiconductor optical amplifier, bulk-SOA)和量子阱半导体光放大器(quantum-well semiconductor optical amplifier, QW-SOA)相比,具有优异的非线性性能,如阈值电流低、微分增益高、温度灵敏性低等,应用前景广阔^[1-5]。全光波长转换技术因具有提高波长利用率、降低网络阻塞率等优点,成为密集波分光网络中关键技术,其中基于交叉增益调制效应(cross-gain modulation, XGM)的波长转换技术实现简单^[6-8]。因此,基于量子点光放大器的交叉增益调制效应的波长转换器一直是研究的重点。啁啾特性在很大程度上会影响QD-SOA的性能,引起传输中信号的走离效应,使误比特率提高^[9-15]。目前对QD-SOA的变换光啁啾问题的详细分析研究还较少,参考文献

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[13] ~ 参考文献[15]中研究了注入电流、线宽增强因子、输入光的功率和波长对变换光啁啾的影响。除了以上影响因素外,本文中进一步分析了抽运光脉宽、抽运光消光比对变换光啁啾的影响,并给出了数值计算的结果。

1 理论模型

QD-SOA 中,载流子在浸润层(wetting layer, WL)、基态(ground state, GS)和激发态(excited state, ES)的三能级跃迁速率方程可表示为^[15-16]:

$$\frac{\partial N_w}{\partial t} = \frac{J}{eL_w} - \frac{N_w(1-h)}{\tau_{w,2}} + \frac{N_q h}{L_w \tau_{2,w}} - \frac{N_w}{\tau_{w,r}} \quad (1)$$

$$\frac{\partial h}{\partial t} = \frac{N_w L_w (1-h)}{N_q \tau_{w,2}} - \frac{h}{\tau_{2,w}} - \frac{h(1-f)}{\tau_{21}} + \frac{f(1-h)}{\tau_{12}} \quad (2)$$

$$\frac{\partial f}{\partial t} = \frac{h(1-f)}{\tau_{21}} - \frac{f(1-h)}{\tau_{12}} - \frac{f^2}{\tau_{1,r}} - \sum_i \frac{L_w g_i(\nu_i) P}{N_q \sigma h_1 \nu_i} \quad (3)$$

式中, N_w 为载流子在浸润层的浓度, L_w 为有源区的厚度, N_q 为表面量子点(quantum dot, QD)的密度,一般为 $5 \times 10^{10} \text{ cm}^{-2}$, J 和 e 分别为注入电流密度和电子的电量, $h(f)$ 为电子在激发态(基态)的占有几率, τ_{21} 为从激发态到基态电子的跃迁时间, τ_{12} 为从基态到激发态电子的跃迁时间, $\tau_{w,2}$ 为从浸润层到激发态电子的弛豫时间, $\tau_{2,w}$ 为从激发态到浸润层电子的跃迁时间, $\tau_{w,r}$ 为浸润层中电子的自发辐射时间, $\tau_{1,r}$ 为量子点内电子的自发辐射时间, $h_i \nu_i$ 为光子能量, ν_i 为第 i 个单模光的频率, g_i 为其对应的模式增益。假设量子点中的电子和空穴是均匀分布的,即 $f_i = f, h_i = h$, 增益简单表示为 $g = g_{\max} (2f - 1)$ ^[2], g_{\max} 为最大模式增益。

在 QD-SOA 中,信号光的光场传输方程可表示为^[17]:

$$\frac{dE^+}{dz} = \Gamma [g(1 - j\eta) - \alpha_{\text{int}}] E^+ \quad (4)$$

$$\frac{dE^-}{dz} = -\Gamma [g(1 - j\eta) - \alpha_{\text{int}}] E^- \quad (5)$$

式中, g 为模式增益, z 为光场的传输方向, E^+ (E^-) 分别是沿着正(反)方向传输的光场强度, η 是波导的线宽增强因子, Γ 是信号光的光场限制因子, $j = (-1)^{1/2}$, α_{int} 是光的损耗系数。(4)式和(5)式的边界条件是:

$$E^+(0) = (1 - r_1) E_{\text{in}} + r_1 E^-(0) \quad (6)$$

$$E^-(L) = r_2 E^+(L) \quad (7)$$

式中, E_{in} 为输入信号的光场强度, L 为量子点有源区的

长度。

由于探测光的自相位调制和抽运光的交叉相位调制的共同作用,变换光的相位沿着光传输方向的变化为:

$$\frac{\partial \Phi}{\partial z} = -\frac{\alpha}{2} \alpha g \quad (8)$$

式中, α 为线宽增强因子。

沿 QD-SOA 有源区长度积分(8)式可得到相位随时间的变化:

$$\Phi(t) = -\frac{\alpha}{2} \left[\int_0^L g(z, t) dz \right] \quad (9)$$

变换光的啁啾为:

$$\Delta \nu = -\frac{1}{2\pi} \frac{d\Phi}{dt} \quad (10)$$

2 数值计算

为了研究 QD-SOA 的啁啾特性,求解(1)式~(5)式,所取参量如表 1 所示。

Table 1 QD-SOA parameters for numerical simulation^[15,18-19]

parameter	value
maximum modal gain g_{\max}	15.0cm
QD-SOA length L	2mm
thickness of wetting layer L_w	0.2 μ m
QD-SOA width W	2 μ m
surface density of QDs N_q	$5 \times 10^{10} \text{ cm}^{-2}$
electron relaxation time from ES to GS τ_{21}	0.16ps
electron escape time from GS to ES τ_{12}	1.2ps
spontaneous radiative lifetime in QD $\tau_{1,r}$	0.4ns
electron escape time from ES to WL $\tau_{2,w}$	1ns
electron relaxation time from WL to ES $\tau_{w,2}$	3ps
absorption coefficient of the material α_{int}	3cm

采用分段模型对 QD-SOA 全光波长转换模型进行数值计算,取分段数 $N = 100$ ^[11],假设 QD-SOA 注入电流为 20mA,抽运光是 1 阶高斯脉冲模拟信号,其速率为 160Gbit/s,半峰全宽(full width at half maximum, FWHM)为 0.24ps,峰值功率 $P_{p,\text{pk}} = 9\text{dBm}$,波长 $\lambda_p = 1500\text{nm}$,探测光功率 $P_c = -20\text{dBm}$,波长 $\lambda_c = 1550\text{nm}$ 。图 1 中给出了波长转换后探测光波形以及

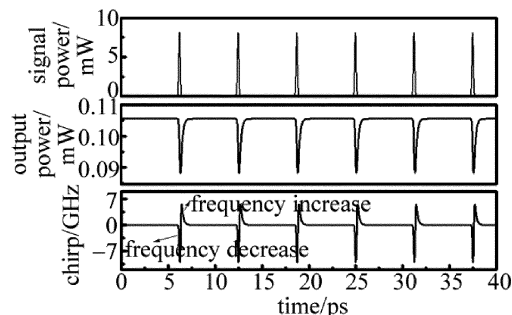


Fig. 1 Converted signal pulse and the associated chirp

对应的啁啾。从图中可以看出,变换光的前沿为负啁啾(其中心频率减小,波长向长波方向移动),变换光后沿为正啁啾(其中心频率增大,波长向短波方向移动),正啁啾值约为 5.48GHz,负啁啾的值约为 -9.97GHz,这是因为变换光脉冲的上升沿时间大于下降沿时间。

图 2 所示是随注入电流的增加,变换光啁啾迅速增大,当电流大于 1.0mA 时,啁啾值趋于平稳。随着注入电流增加,量子点中的载流子密度迅速增大,使得抽运光增益变大,抽运光对载流子密度有更大的调制,导致折射率的变化更大,进而变换光的啁啾增大。但随着注入电流继续增加,量子点中的载流子密度趋于饱和,啁啾值基本不再变化。

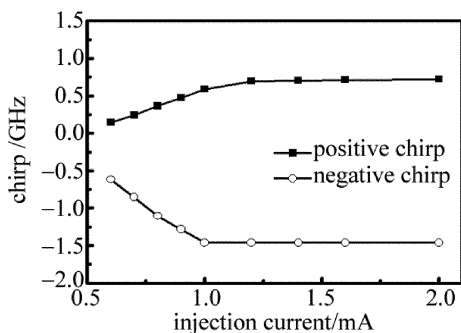


Fig. 2 Chirp of converted signal vs. injected current

图 3 所示是不同抽运光脉宽下啁啾随时间的变化。从图中可以看出,变换光啁啾随着抽运光脉冲宽度的增加而减小。当抽运光脉冲宽度从 0.3ps 逐渐增加到 1.2ps 时,变换光的啁啾曲线从尖锐趋于平坦,啁啾值逐渐减小。当输入脉冲序列的码速率一定时,抽运光的脉宽较宽时,变换光的啁啾值较小;脉宽较窄时,采用 XGM 全光波长转换器变换光的啁啾值较大。

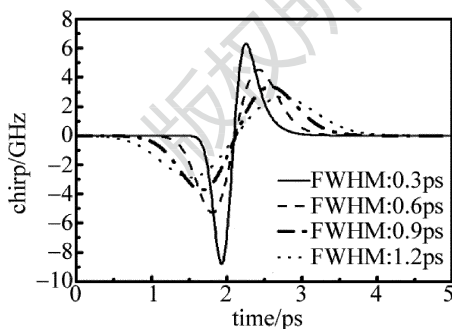


Fig. 3 Temporal chirp under different pump pulse width

图 4 中进一步分析了抽运光脉冲宽度对变换光啁啾的影响,如图所示,变换光啁啾随着抽运光脉冲宽度的增加而减小。这是因为在相同的单脉冲能量下,抽运光脉宽越小,量子点中载流子密度的变化越快,使得变换光的啁啾越大。

图 5 所示是不同抽运光消光比 (extinction ratio, ER) 时啁啾随时间的变化。当抽运光消光比为 11.3dB,

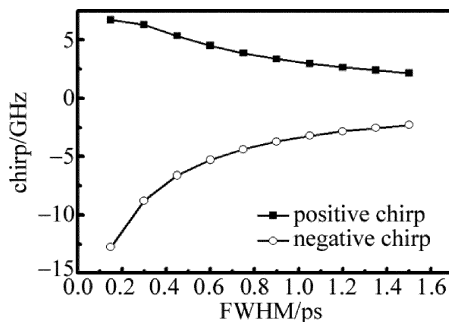


Fig. 4 Chirp of converted signal vs. pump pulse width

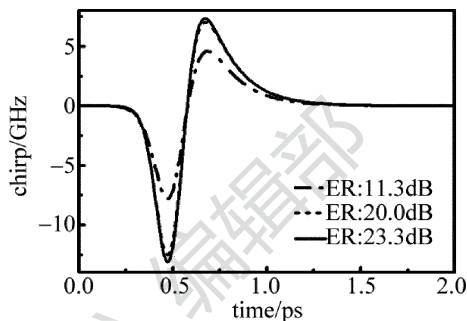


Fig. 5 Temporal chirp under different pump extinction ratio

20.0dB, 23.3dB 时,变换光的正啁啾为 4.59GHz, 7.14GHz, 7.33GHz;负啁啾为 -7.83GHz, -12.72GHz, -13.14GHz。变换光啁啾随着抽运光消光比的增加而增大。因此,在设计基于 XGM 调制的 QD-SOA 时,要考虑抽运光消光比和信号光啁啾的均衡。

图 6 更清楚地显示出变换光啁啾随抽运光消光比的增加而逐渐增大,这是因为在相同的单脉冲能量下,抽运光 ER 越大,信号“1”的功率越大,信号“0”的功率越小。随着抽运光 ER 增大,当输入信号“1”时,量子点中的载流子密度变化更剧烈,得到变换光的啁啾就越大。但当抽运光 ER 超过 20.0dB 后,信号“1”峰值功率变化不大,啁啾变化趋于缓和。

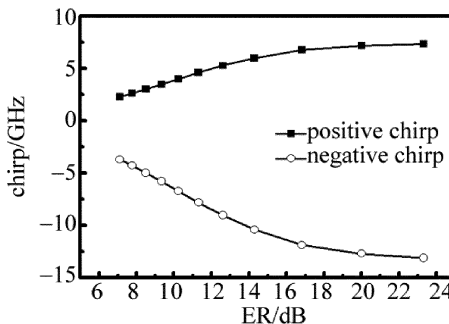


Fig. 6 Chirp of converted signal vs. extinction ratio of pump light

3 结论

基于 XGM 全光波长转换原理,利用建立的动态仿真模型完成全光波长转换,详细分析了 QD-SOA 注入电流、抽运光信号脉宽、抽运光消光比对变换光啁啾的影响。计算结果显示,增大注入电流使变换光啁啾

增大,增大抽运光信号脉宽会减小变换光啁啾值。此外,增大抽运光消光比使变换光啁啾增大,设计 QD-SOA 时需要注意二者的均衡。变换光啁啾效应是密集波分全光网络应用量子点光放大器的交叉增益调制效应类型的全光波长转换器的主要障碍,实际应用中对于这一方案的变换光必须考虑啁啾效应的影响,以减小误比特率。

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