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## 164W LD侧抽运准连续Nd:YAG/HGTR-KTP高功率绿光激光器

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**摘要:** 为了研究百瓦级高光束质量绿光激光器, 采用激光二极管侧面抽运双棒串接、双声光调Q的方法, 依据光束传输矩阵, 分析比较了V型折叠腔内分别置入单、双激光晶体时, 其热透镜效应对谐振腔稳定性、折叠臂内光场分布以及倍频晶体处子午光斑和弧矢光斑大小的影响, 倍频晶体选用具有抗灰迹特性的II类临界相位匹配KTP晶体。当总抽运功率为1200W、重复频率为27.2kHz时, 得到了脉冲宽度为130ns的164W准连续绿光输出, 光光转换效率为13.7%, 光束质量因子 $M_x^2 = 10.46, M_y^2 = 10.59$ 。结果表明, 使用双棒串接、双声光调Q V型腔结构, 可以获得百瓦级高功率、高光束质量532nm绿光输出。

**关键词:** 激光器; 高功率激光; 双棒串接; 热透镜效应

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## 164W side-pumped quasi-continuous-wave Nd:YAG/HGTR-KTP green laser

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**Abstract:** In order to investigate more than one hundred Watt green laser, two serial rods pumped by laser diodes and two Q-switched V-shaped resonators were used. Based on the transmission matrixes, when single and double rods were placed in the cavity respectively, the stable condition of cavity, the light distribution in the folded arm, along with the sagittal and tangential spot size on the nonlinear crystal influenced by the thermal lens effect were analyzed and compared. A high gray tracking resistivity (HGTR)-KTP crystal with type II critical phase-matching was adopted as intracavity frequency doubler. When the pump power of two diode lasers was 1200W and the repetition rate was 27.2kHz, 164W green laser with the pulse width of 130ns was obtained. The optical-optical conversion efficiency was 13.7%. The beam quality factor was  $M_x^2 = 10.46, M_y^2 = 10.59$ . The result shows that one hundred Watt green laser could be obtained in the two-rod and two Q-switched V-shaped resonator configuration.

**Key words:** lasers; high power laser; two serial rods; thermal lens effect

### 引言

激光二极管抽运的全固态激光器具有体积小、效率高、稳定性好和寿命长的特点, 在医疗、科研、通讯、国防、工业加工等领域有着广阔的应用前景, 国内外学者对此进行了广泛的研究<sup>[1-5]</sup>。特别是近几年来, 随着千瓦级LD阵列的出现, 利用非线性晶体进行激光器腔内外倍频、和频、光参量振荡等技术获得高功率短波

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长激光已成为激光领域中研究的热点, 其中, 最为瞩目的就是全固态百瓦级绿光激光器的研制<sup>[6]</sup>。

尽管激光二极管抽运的全固态激光器与传统的灯抽运激光器相比, 具有高效、长寿命、体积小、热效应小等优点, 但高功率运转下, 激光晶体的热透镜效应对谐振腔稳定性、功率输出、转换效率及光束质量等产生的负面影响仍然是激光器件应用研究的重要课题。关于解决激光器热透镜的问题, 除可以设计不同几何构型的增益介质外, 还可以通过腔内插入附加的光学元件或同时采用完全相同的双激光晶体来对热透镜效应进行补偿<sup>[7-13]</sup>。作者通过采用双棒串接V型腔结构, 在讨论谐振腔内单、双激光晶体热透镜效应对谐振腔稳定性、束腰半径等参数影响的基础上, 设计了大抽运功

率变化范围内双 Nd:YAG 串接 V 型热不灵敏腔, 最大获得了 164W 的 532nm 绿光激光输出。

## 1 理论分析与计算

在腔内倍频的情况下, 折叠腔具有有效空间大、模参量调整灵活等特点, 很容易实现腔内双向倍频单向输出, 而且还可以使倍频转换过程与激光晶体隔离, 这样不仅可以减少激光晶体对倍频光的吸收, 还可以提高倍频转换效率, 在一定程度上减缓激光器运转过程中的热透镜效应, 因此, 折叠腔结构被很多腔内倍频激光系统所采用。本文中所讨论的激光二极管抽运的双棒串接放大器输出 (amplifier output, AO) 双声光调 Q Nd:YAG/KTP 激光系统就采用了 V 型谐振腔结构, 其实验装置图及其热透镜等效光路图见图 1 和图 2。

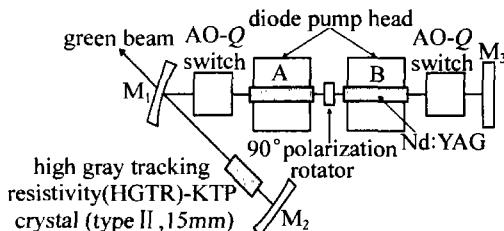


Fig. 1 Schematic drawing of the cavity configuration

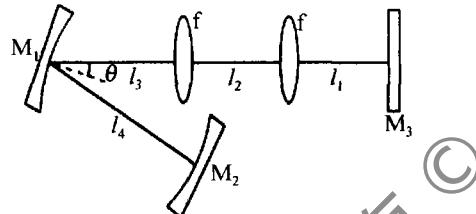


Fig. 2 Equivalent thermal lens resonator

假设两个激光晶体的物理性质和光学性质完全相同且具有相同的热焦距。以端镜  $M_3$  为参考面, 则谐振腔内的单程传输矩阵为<sup>[5]</sup>:

$$M_s = \begin{bmatrix} a_s & b_s \\ c_s & d_s \end{bmatrix} = \begin{bmatrix} 1 & l_4 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -2\cos\theta/R_1 & 1 \end{bmatrix} \begin{bmatrix} 1 & l_3 \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ -1/f & 1 \end{bmatrix} \begin{bmatrix} 1 & l_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1/f & 1 \end{bmatrix} \begin{bmatrix} 1 & l_1 \\ 0 & 1 \end{bmatrix} \quad (1)$$

$$M_t = \begin{bmatrix} a_t & b_t \\ c_t & d_t \end{bmatrix} = \begin{bmatrix} 1 & l_4 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -2/R_1 \cos\theta & 1 \end{bmatrix} \begin{bmatrix} 1 & l_3 \\ 0 & 1 \end{bmatrix} \times \begin{bmatrix} 1 & 0 \\ -1/f & 1 \end{bmatrix} \begin{bmatrix} 1 & l_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -1/f & 1 \end{bmatrix} \begin{bmatrix} 1 & l_1 \\ 0 & 1 \end{bmatrix} \quad (2)$$

$G$  参量因子为:

$$G_1 = a_i - \frac{b_i}{R_2}, G_2 = d_i - \frac{b_i}{R_2}, (i = s, t) \quad (3)$$

谐振腔稳定条件为:

$$0 < G_1 \times G_2 < 1 \quad (4)$$

式中, 下角标  $s, t$  分别代表弧矢面和子午面,  $R_1, R_2, R_3$

分别为谐振腔镜  $M_1, M_2, M_3$  的曲率半径,  $\theta$  为腔内光束在折叠镜  $M_1$  上的入射角,  $f$  为激光晶体热焦距。

根据上述条件, 用计算机做数值计算处理有关数据, 首先筛选出一组较为理想的谐振腔参量:  $l_1 = 9\text{cm}$ ,  $l_2 = 5\text{cm}$ ,  $l_3 = 8\text{cm}$ ,  $l_4 = 16\text{cm}$ , 折叠角(半角)  $\theta = 14^\circ$ , 在此基础上, 讨论热透镜效应存在时谐振腔稳定运转条件下各参量的变化情况。

图 3 为谐振腔  $G$  参量随热焦距的变化规律图。

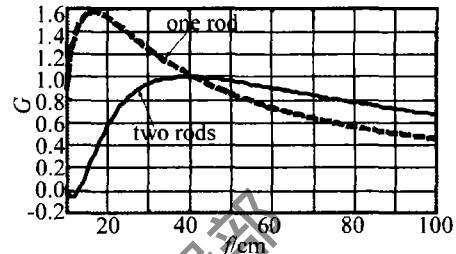


Fig. 3 The cavity stability of single and double laser crystals

为了方便比较, 在其它条件完全相同的情况下, 分别做出双激光晶体及去掉左激光晶体后的稳区图。从图 3 可以看出, 利用双激光晶体补偿后, 谐振腔的稳区范围明显加宽, 双激光晶体的热焦距在  $[12\text{cm}, \infty)$  范围内变化时, 谐振腔始终能满足腔的稳定性条件, 宽的稳区范围更有利高功率激光的输出。

对于 V 型谐振腔而言, 为保证倍频效率的提高, 一般把倍频晶体放在折叠臂的光腰处, 并且要求腔内光场的像散要尽量小, 以获得高质量激光输出。从图 4a 和图 4b 可以看出, 图 4a 中双激光晶体折叠臂内子

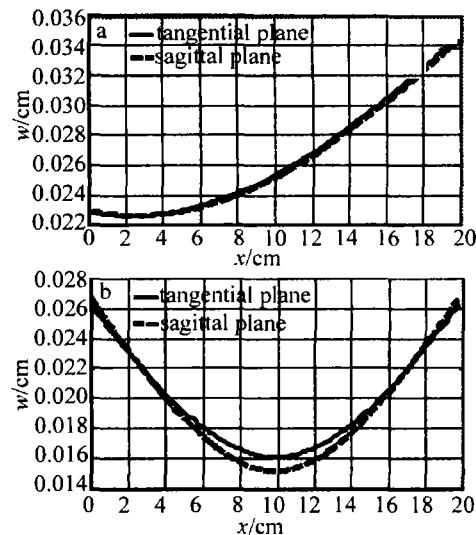


Fig. 4 a—the light distribution in folded arm for dual laser crystal cavity  
b—the light distribution in folded arm for single laser crystal cavity

午面光斑半径与弧矢面光斑半径重合得更好, 而且束腰半径在靠近谐振腔端镜  $M_2$  处, 而图 4b 中单激光晶体谐振腔内折叠臂的束腰半径在折叠臂中间处, 且像散较大。从实际操作角度出发, 倍频晶体靠近端镜  $M_2$  处可使光路调节更为灵活方便, 可以避免折叠臂内光

学元件对光路的遮挡,从而使折叠半角取值范围更大。

图5a和图5b分别为双激光晶体与单激光晶体谐振腔中倍频晶体处子午面和弧矢面光斑尺寸大小随激光晶体热焦距的变化关系图。结果表明,双激光晶体

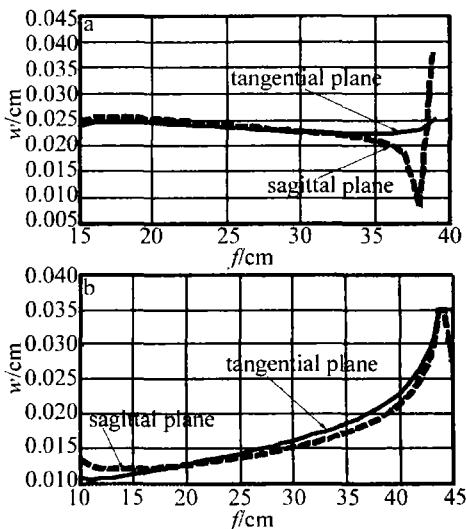


Fig. 5 a—the wave radius on SHG crystal in the dual laser crystal resonator  
b—the wave radius on SHG crystal in the single laser crystal resonator

谐振腔内子午面和弧矢面的光束光斑尺寸大小在高功率下重合得较好,而在单激光晶体谐振腔内二者差异较大且随热焦距的改变变化较为显著,可见前者更易于高功率抽运条件下获得高质量的绿光激光光束。

## 2 实验装置与结果

图1所示的实验装置中,两个型号相同的半导体激光抽运组件串接且同步驱动。每个组件由30个20W的LD组成,按照五角形等间距侧面抽运Nd:YAG晶体棒,总抽运功率1200W。Nd:YAG棒的尺寸均为 $\varnothing 5.0\text{mm} \times 105\text{mm}$ ,倍频晶体HGTR-KTP具有抗灰线特性,采用II类临界相位匹配方式( $\Phi = 23.8^\circ$ ,  $\theta = 90^\circ$ ),并实施恒温控制,在一定程度上补偿了因热效应引发的倍频晶体相位失配。调Q方式采用正交放置、同步驱动的双声光调Q模块以实现在高功率激光运转下声光所具有的较高的关断能力,增大基波脉冲的峰值功率,提高倍频转换效率。平凹镜M<sub>1</sub>凹面镀1064nm高反与532nm增透的双色膜,平面镀532nm增透膜;平凹镜M<sub>2</sub>凹面镀1064nm与532nm双色高反膜;平面镜M<sub>3</sub>内表面镀1064nm与532nm双色高反膜。

图6是532nm绿光激光输出功率随抽运电流的变化关系。由图可知,随着抽运功率的增大,绿光输出功率逐渐升高,当两块半导体模块的总抽运功率为1200W,重复频率为27.2kHz时,获得了532nm绿光最大平均输出功率为164W,脉冲宽度为130ns,见图7。整个过程中,激光系统都在稳定状态下运转。在输出

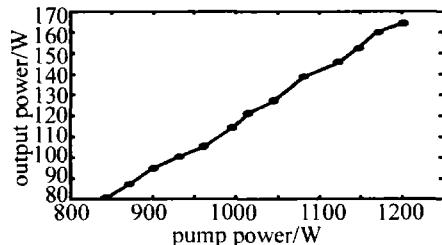


Fig. 6 Green laser output power vs. different pump power of diode-laser module

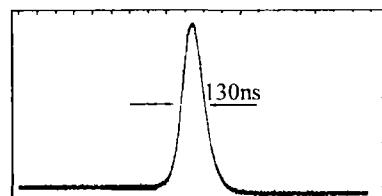


Fig. 7 The pulse width of 532nm green laser

功率为164W时,使用美国Spirecon公司生产的LBA-200光斑测试仪,测得光束质量因子 $M_x^2 = 10.46$ , $M_y^2 = 10.59$ 。激光器连续工作2h以上,每隔15s测量1次输出功率,输出功率不稳定度小于2.3%。

## 3 结论

通过讨论谐振腔内单、双激光晶体热透镜效应对谐振腔稳定性、腔内光场分布及束腰半径等参量的影响,设计了双Nd:YAG串接热不灵敏腔,采用激光二极管侧面抽运双Nd:YAG晶体II类临界相位匹配HGTR-KTP晶体腔内倍频的方案,最大获得了单端输出164W的532nm绿光激光。

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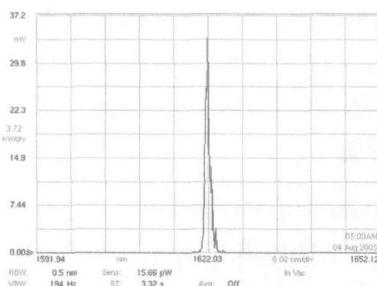


Fig. 5 Signal spectrum of 1662nm of PPMgLN-OPO

### 3 结论

实验中采用二极管端面抽运 1064nm 声光调  $Q$  Nd:YAG 激光器作为抽运源, 研究了 PPMgLN-OPO 的温度调谐特性和输出特性。当温度从 40℃ 升高到 200℃ 时, 获得了 1565nm ~ 1670nm 宽调谐信号光输出, 实现了全固态抽运的光参量振荡的宽调谐输出; 当晶体的温度为 110℃, 抽运光平均功率为 1.61W,  $Q$  开关的重复频率为 10kHz, 脉宽为 70ns 时, 获得了 211mW 波长为 1.631μm 的信号光输出; 随着温度的升高, 输出信号光平均功率缓慢增大, 并且在室温下实现了参量光输出, 晶体没有受到损伤, 证明了掺氧化镁铌酸锂晶体抗光损伤能力提高了。实验结果表明, 温度调谐光参量振荡器可以作为宽波段的可调谐相干光源。

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