

# Optical fiber grating sensors for height measurement of liquid

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Abstract: A precision approach utilizing fiber grating as elements to measure height of liquid is presented and experimented and the basic issues of the sensor system design are discussed. This t ype of sensor can be used in precision measurement of medium measurement ranges. The sensitivity of 0. 15mm/ pm for measuring the height of water has been obtained.

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# Introduction

版权所有 © 《激光技术》编辑部 Compared with temperature and pressure measurement, the methods to measure the height of liquid are not good enough. In some circumstances, such as the liquid surface is fluctuating, the liquid is boiling and there are small floating materials on the liquid surface, it is difficult to measure the height of liquid precisely. Nowadays, there are several methods to measure the height of liquid. For example, using a rule to measure the height of liquid directly, measuring the height of liquid through the variation of the buoyant force or through the variation of liquid pressure or through the variation of electrical capacity induced by the liquid height variation. Because the precision of the transferring from these variations to electrical variation is not high, the sensitivity of measuring the height of liquid is not better than 1mm. Because of the immeasurable ranges, the technology of liquid height measurement needs to be developed a lot. It is a very important task to find more precision and higher resolution methods to measure the liquid height  $[1,2]$ .

Recent years a number of papers have been reported on research of optical fiber grating sensors, most of which are used to measure strain, temperature and pressure<sup>[3~9]</sup>. In this paper, we experiment primarily and present an in-fiber grating application of measurement the height of liquid. This type of optical fiber grating sensors may be used in electron-magnetic interference or/ and inflammable or/ and corrosive or/ and conducting or/ and foaming surface liquids. Because a

floating bar is used to transfer the liquid height to the strain of an in-fiber grating, the corresponding issues of design, including the measurement range, sensitivity, the diameter and length of the floating bar etc. , are discussed. As the method we present is to embed the in-fiber g rating element into the measured liquid, the fluctuation and the foam of the liquid surface w ill not influence the measurement precision and the immeasurable range can be reduced by using a short in-fiber grating. Our sensors fit with high precision of measurement range of a few hundred millimeters.

## 1 Experimental configuration

T he experimental arrang ement is shown in Fig. 1. A hollow floating bar FB is hung by spring SP so that the w eight of FB is balanced. A broadband light source illuminates, through an



Fig. 1 Arrangement for liquid measurement utilizing fiber gratings

isolator IS and a 3-dB coupler, the fiber w ith a in-fiber Bragg gratings G, of w hich the nominal reflecting w avelength is 1549nm. The reflecting signal from the grating is detected with a spectrum analyzer SA ( or w ith other interrogative approaches) , the height variation of liquid is measured w ith a ruler R. One end of the fiber grating G is mounted to the center of the round surface of the lower end of the bar while the other end of G is firmly fixed to the unmovable shelf. T he spring supported on the shelf is so placed that it can be moved up and down to pre-strain G

with a small quantity. We also employed a spring system consisting of a principal spring SP and 4 side-springs ( four rubber ropes) to stabilize the floating bar  $(Fig. 2)$ .

The buoyant force  $F$  acting on the FB can be presented as

$$
F = \pi r^2 \rho \Delta h \tag{1}
$$

FB is balanced. A broadband Fig. 1 Arrangement for liquid measurement stillating<br>rece illuminates, through an gradings<br>with a in-fine Transg gradings G, of which the now we dength is 1549mm. The reflecting signal from the Where, r is the radius of the floating bar,  $\rho$  is the density of the liquid,  $\Delta h$  is the variation of liquid height, which can be measured with the ruler R. F increases with the increase of  $\Delta h$ , which induces the reflecting waveleng th shift w ith a proportional quantity. During the experiments, the change of temperature of water is maintained w ithin 0. 1  $\mathbb{C}$ , the reflecting w avelength shift of G w as measured with the spectrum analyzer and the w ater height was recorded w ith the ruler R as

the w ater w as poured into the vessel.

### 2 Experimental results

The experimental results are illustrated in Fig. 3, in which the curve  $A$  is for one spring SP and curve  $B$  is for the principal spring SP with the four side-springs together. Comparing the two curves, we see tw o parallel lines that have illuminated the same hig h linearity and sensitivity in the two cases, although the side-springs which protect the grating from breaking can strongly



Fig. 2 Principal spring and four side-springs

keep the floating bar stable. The sensitivity of 0. 15mm/ pm has been obtained for a fiber grating made of 145Lm diameter KIST-1104 fiber and a floating bar with 36. 0mm diameter. We can ex press the sensitivity as  $K_{w} = 0.00619 \text{pm/nm} \cdot \text{mm}^{2}$ , which gives the reflecting w avelength shift against per mm of height change and per mm 2 of section area. With the spectrum





#### 3 Considerations in design

Five issues have to be considered to design an in-fiber grating liquid height sensor: the max imum limitation of the reflecting w avelength shift  $\Delta\lambda_{\text{max}}$ , which is dependent on the force stretching the optical fiber safely; measurement range  $\Delta h_{\text{max}}$ ; length L and section area A of the floating bar; sensitivity  $K$  and resolution. The relation of these parameters can be expressed by



Fig. 4 Floating bar: length and diam eter

$$
K_{w} \mathcal{P} \mathcal{A} h = \Delta \lambda < \Delta \lambda_{\text{max}} \tag{2}
$$

Where,  $K_{w} \rho$  is the sensitivity of liquid,  $\Delta \lambda$  is the reflecting wavelength shift w hich can not be greater than  $\Delta \lambda_{\text{max}}$ , A is the section area of the floating bar. For a bar with a round section  $(Fig. 4)$ , Eq.  $(2)$  can be rew ritten as  $K_w \rho \pi r^2 h = \Delta \lambda < \Delta \lambda_{\text{max}}$  (3) Where,  $r$  is the radius of the floating bar, and

 $S = K_{\rm w} \Omega_1 = K_{\rm w} \Omega_1 r^2 = \Delta \lambda_{\rm max} / h_{\rm max}$  (4)

is the sensitiv ity of measurement w hich is directly proportional to  $\rho$  and A.  $\Delta \lambda_{\text{max}}$  varies with different

types of fiber. Wang has indicated that  $\sim$  7800pm reflecting w avelength shift can be induced by stretching a fiber of  $\sim 130$ <sup>L</sup>m diameter with 7N force, the corresponding strain is 7860<sup>Li</sup>stain beyond which the fiber will be snapped $^{\rm [10]}$  . These are the maximum limitation of the wavelength shift, strain and stretching force acting on the optical fiber. In order to be safe, it is appropriate to limit the greatest w avelength shift to  $\Delta \lambda_{\text{max}} \approx 5000 \text{pm}$  which correspond - 5nm to a ~ 5nm w aveleng th shift. One can use the given measurement range  $h_{\text{max}}$  to calculate r then S, or on the contrary use the given S to calculate  $h_{\text{max}}$  and r. The measurement ranges of traditional types are 0  $\sim$  300mm and 0  $\sim$  2000mm et al. We chose  $h_{\text{max}} = 500$ mm as a measurement range of the example design, which needs the length of floating bar  $L > 500$  mm (for example 550 mm). From Eq. ( 3) the diameter of the floating bar in w ater height measurement can be calculated as below

$$
\Delta \lambda_{\text{max}} = K_{\text{w}} \, \rho_{t_{\text{max}}} \pi r^2 \tag{5}
$$

As discussed above we take that  $\Delta\lambda_{\rm max}$  = 5000pm,  $h_{\rm max}$  = 500mm,  $\rho = 1$ g/ cm<sup>2</sup> and  $K_{\rm w}$  =

 $0.00619$ pm/mm $^{\bullet}$ mm $^2$ thus 5000pm  $\approx$  (0.00619pm/mm  $\cdot$  mm<sup>2</sup>)  $\times$  500mm  $\times$   $\pi r_w^2$ Which means  $r_w \approx 22.68$ mm and the diameter is 45.36mm

In a word, it is safe for a fiber grating of  $\sim 140$ <sup> $\mu$ </sup>m diameter stretched by a floating bar of 45. 36mm diameter to measure the w ater heig ht of 500mm.

For other liquids,  $r = r_w / \sqrt{\rho}$ 

From Eq. (4), we know that the sensitivity  $S = 10$ pm/mm.

T he resolution varies w ith the interrog ative approaches because they have different w aveleng th shift resolution. For the given example, 10pm w avelength shift is against 1mm water height change. The ordinary resolutions are: 10mm for a spectrum analyzer with a w aveleng th resolution of 0. 1nm; 0. 4mm for a fiber Fabry-Perot filter w ith 4pm w avelength resolution; and 0. 1mm for the approach of length-tuning reference fiber grating.

#### 4 Conclusion and discussion

A novel approach to measure w ater heig ht w as presented and demonstrated. As the in-fiber g rating is embedded into the measured liquid, the measurement precision is immune to the fluctuation of the liquid surface and the foam on the liquid surface. The sensitivity of 6. 49pm/ mm of w ater height measurement has been obtained for a floating bar of 36mm diameter (or  $K = 0.00619$ pm/mm $^{*}$ mm<sup>2</sup>). The sensitivity of the technology of interrogating w avelength shift has achieved 1pm. The sensitivity of 6. 49pm/ mm means the sensitivity of 0. 15mm of liquid height. During the experiments, we maintained the variation of temperature less than  $0.1^{\circ}$ C. A g eneral design consideration fitting for various liquids was given. By calculating, the influence of the wavelength shift induced by w ater pressure under 500mm depth is small, at an order of 0. 015pm, therefore it can be neg ligible. The temperature variation can be compensated by some methods and using a shorter in-fiber grating can reduce the minimum measurable heig ht.

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